

N. Woodland Rd. Sec. A

Russell Twp.

104

FIELD BOOK

1312

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON O.
PHONE 256-.

Book 104

North Woodland Road - No. 16

Sections B & C

Align. - pg. 3-6 Pg 71

Topo - pg. 7-13

X-Sections - pg. 14-28

Culverts - pg. 29-30

Grades - pg. 32-54

FAIRMOUNT RD #16 Sec C & D
Profile & Sect'ns 1950 pgs 57-68

Preliminary Survey of land of L. Williams on
FAIRMOUNT RD CH #16 SEC North Side for
PROPOSED ADDITION to BRIAR HILL & RIVERSIDE Cemeteries
Pg 74

10

FILL RIGHT	AREA		CUBIC YARDS	
	EXCAVA	EMBANK.	EXCAVA.	EMBANK.

Vol. D, Page 558 Road Records
 Road Reduced to 45' from Fuller's
 Mill in Newbury Westerly through
 Russell Tract. to W. line of Township.

Vol. D. P. 536, Road Records
 Wly. from Fuller's Mills to W. line
 of Russell Tract.

Fig. at Grouplin 20" X 1"

- W.	7 ch.
- S. 75° W	2.50 ch
- S 68 1/2° W	7.65
- S 84 1/2° W	11. ch
- N 53° W	20.44 to S. line lot 5.
- W	45.74 ch.
- N 69 1/4° W	7.50
- S 77 1/2° W	3.50
- S 48 1/2° W	2.50
- N 89° W	77.25
- S 63° W	2.50
- N 74 1/2° W	3.67
- W.	61.63
- N 89 1/2° W	81.64
- W	11. ch. to brook through lot 1.
- S 75° W	2.50
- N 71° W	2. ch. to S. line lot 1.

over

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.

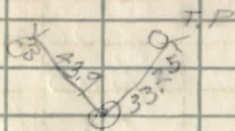
-	N	89 1/2° W		41.42	ch.		
-	S	61° E		10.80	to West line		

of Russell Twp.

We find that the S. line of
lots 1, 2, 3, 4 + 5 is not straight,
but Angling from Corner to Corner.

Royal Burton, Surveyor.

June 14, 1876.



FILL	AREA		CUBIC YARDS	
	RIGHT	EXCAVA	EMBANK.	EMBANK.

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR
						LEFT OR RIGHT

Stakes set on Offset

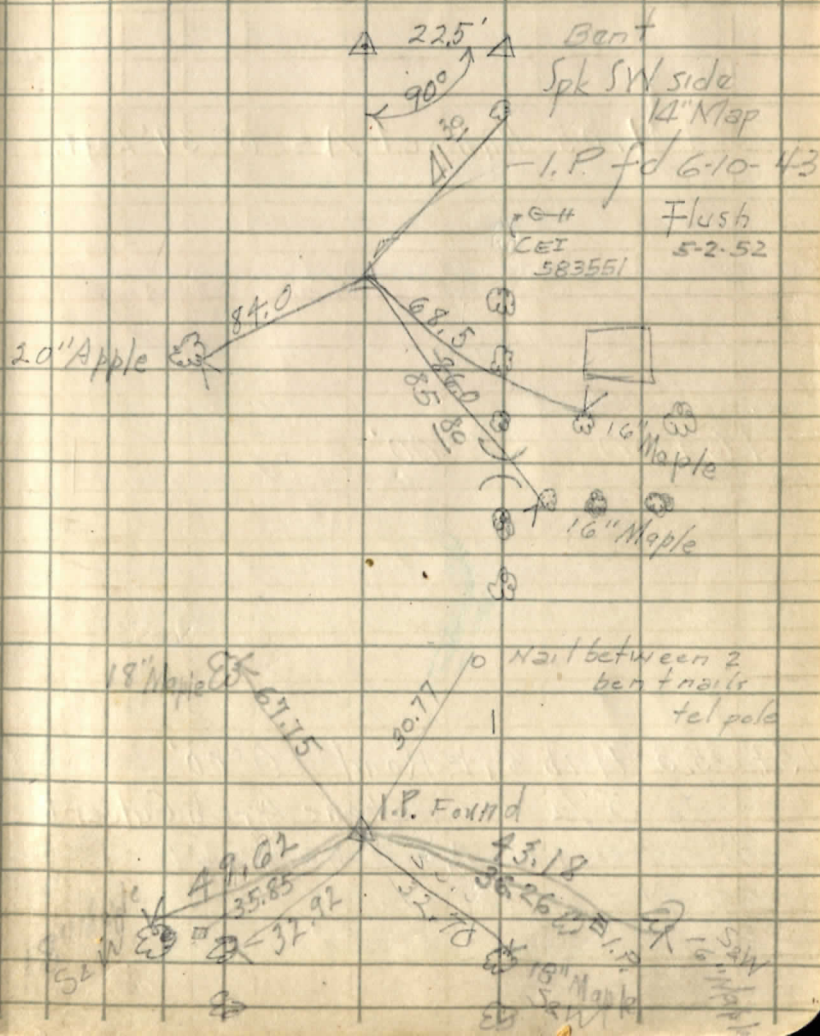
12+00 Hub, set $\Delta = 0^{\circ}00'$

10+00 Hub, set $\Delta = 0^{\circ}38'$ Right

0+00 \pm N+S. Road between Hunting Valley Village + Russell Twp.

FILL	AREA	CUBIC YARDS
RIGHT	EXCAVA EMBANK.	EXCAVA. EMBANK.

of 22.5' from E.
 May 20, 1927, Marks, Grad, D. Parks



STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.

39+99.72 (1952)

40+00 Hub. 0°00'

22+41.0 Hub set Δ = 0°39' Left.

16+00 0°00'

15+05.3 Hub on Road 0°00'
5 1/2 Ft. Stone Arch Culvert

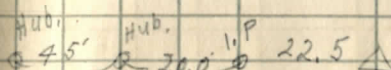
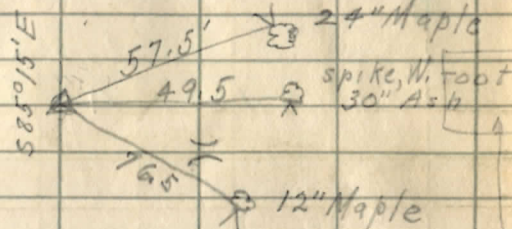
FILL	AREA		CUBIC YARDS	
	RIGHT	EXCAVA	EMBANK.	EMBANK.

Pipe & Ref.

points fd

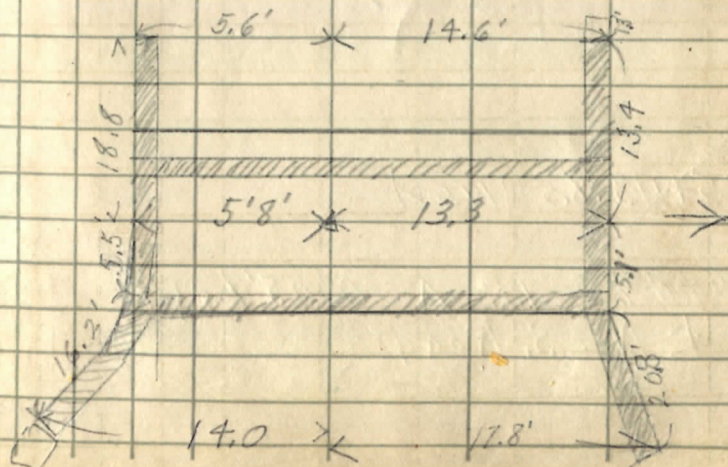
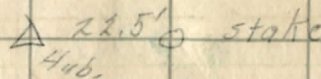
6-10:43 Dist
notched.

Fd Flush May '52



500 pg. 56 for
1946 } Ref
1952 }

House



STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.

82+50 Hubset $\Delta = 0^{\circ}00'$

6/27

76+37.3 Oldstone Found. Section Corner
 $\Delta = 0^{\circ}40'$ Left

$$\begin{array}{r} 76+37.3 \\ 55+44 \\ \hline 2093.3 \end{array}$$
 m 1952
 2092.2

55+43.80 (1952)

55+43.80 I.P. $\Delta = 0^{\circ}05'$ Left
 E N + S. Road (Lovers Rd)

10 penny nail S side
 6" every 7'

FILL	AREA		CUBIC YARDS	
	RIGHT	EXCAVA	EMBANK.	EMBANK.

I.P. Fd Flush
 July '46
 See pg 71

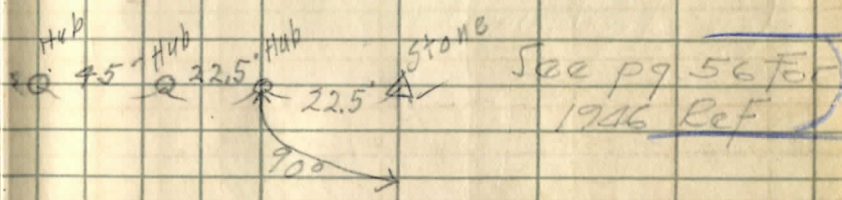
Box 87

38.0

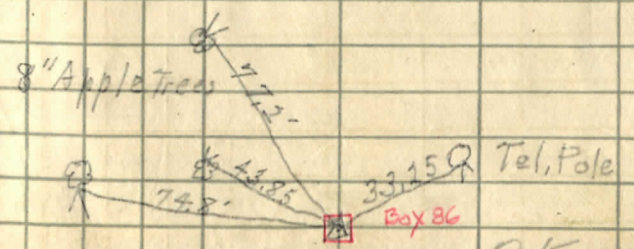
CHIMNEY

36" Ash

May 27, 1927 - Marks, Gray, Spahn



7-



OK 1946
 May 52 see new ref
 on pg 71

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR
						LEFT G.

117+23.8 Iron Pipe, \pm Chillicothe road
2.220 miles

116+0 = I undtane approach

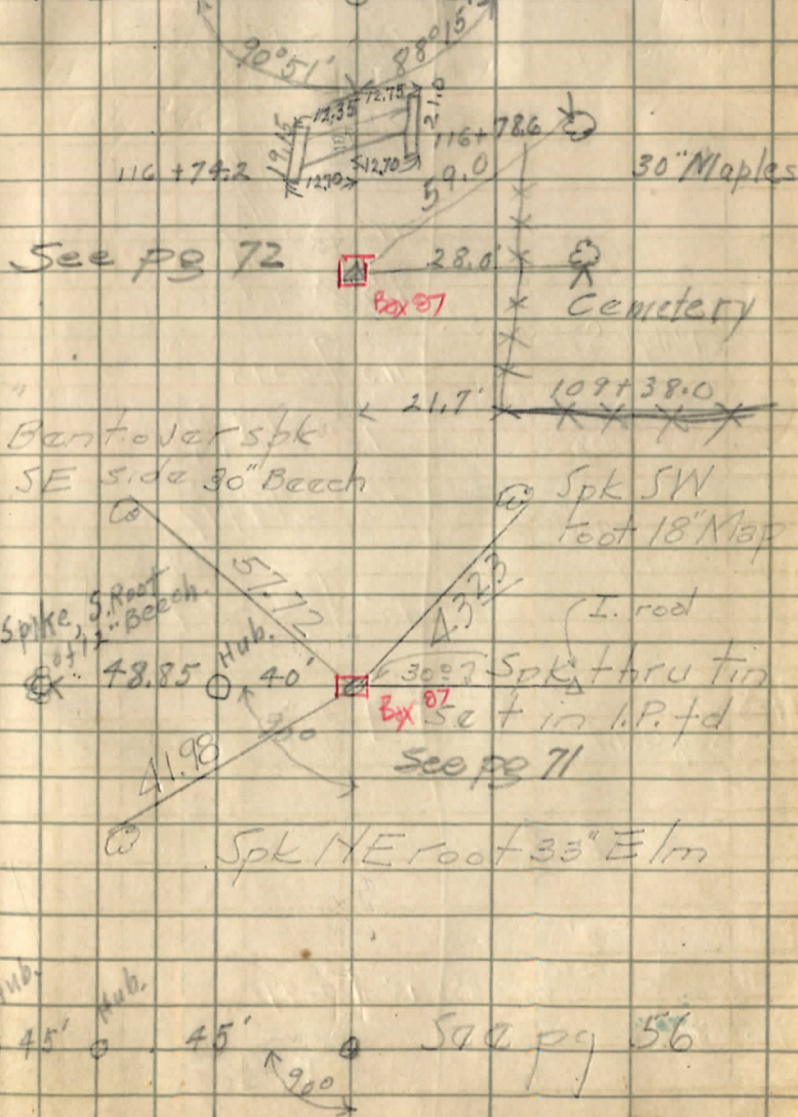
112+00 Hub set $\Delta = 0^{\circ}00'$

96+00 - Hub. Set $\Delta = 0^{\circ}00'$

88+50 Hub. set $\Delta = 0^{\circ}00'$

FILL	AREA		CUBIC YARDS	
RIGHT	EXCAVA	EMBANK.	EXCAVA.	EMBANK.

~~Chillicothe Rd.~~

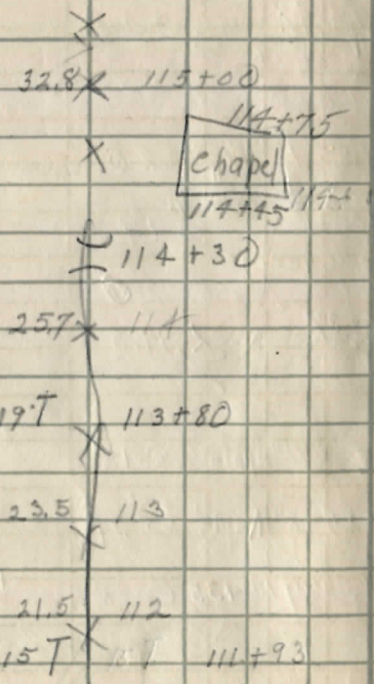


STA.	B. S.	H. I.	F. S.	ELEV.	GRADE	CUT OR	
						LEFT	G.
		85+00	Valley				
					84+00		
		88+36	T 13'			85+85	
						88+14	
					55'	82+85	
		82+45	16.5				
					33.5	82+33	
		81+55	T 14.5				
		80+40					
		79+79	T 14.5				
		77+73	T 18.0				
		76+37.3					
							Sec. Line
		76+33	23.5				
		75+10	T 19.0				
		75+00	23.0				
		74+42					
		73+48	T 18.0				
		73+00	20'				
		71+51	T 18.0				
		69+49	T 18'				
		68+31	21.0				
		68+12					

FILL	RIGHT	AREA		CUBIC YARDS	
		EXCAVA	EMBANK.	EXCAVA.	EMBANK.
			13.2' x 14.6'		2' 9" x 3' 0" Stone Box Good Condition
		93+60.7'		22.0	T 93+63
		12" Elm 93+27	19.0		
		15" W. Cher 92+29	19.5	25.5	92+50 15" Apple
		15" Syc. 92+25	27.5		
		15" W. cherry 92+05	15.5	20.5	T 91+51
		24" Beech 91+65	21'		
		91+11 24" Maple	22.5		
		90+95 18" Maple	19.5		
		90+67 24" Maple	39'		90+67 P.L. 3
		90+48 30" Maple	32.5		
		90+18 30" Maple	32.5		
		88+68 18" W. cherry	15.0	15'	T 89+35
		24" W. Cherry 87+98	14.5		
		87+23.5		11.0	2.8
		1' x 1' Stone Sluice Floor			
		85+71			
		15" Cherry 85+54	16.0	20.5	T 85+35
		85+28	18.0		

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR		FILL	AREA		CUBIC YARDS	
						LEFT	C.		RIGHT	EXCAVA	EMBANK.	EXCAVA.

115+75 30" Maple 20.5



15" W Ch. 110+55 @ 19

15" W Ch 110+35 @ 18

19.5 T 109+95

109+87 10" Maple 17.5

109+67 15" W Ch @ 19

109+30 15" W Ch @ 19

9d
2.0

0
6
ed

16.2
2.5

5
te

#

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
8	8.11	1039.31		1031.20			
117+24			10.8	1028.5			
117+80			10.3	1029.0			
117+59			11.2	1028.1			
117+31			10.25	1029.06			
117+23.8			10.12	1029.19			Chilliothe Road
117+17			10.25	1029.06			
117			9.0	1030.3			
116+50			7.7	1031.6			
116			3.4	1035.9		10.4 11.7 14.0 13.2	
						6.0 5 4.5 4.0	
115	10.15	1048.97	0.49	1038.82		6.9 4.4 3.0	
			4.7	1044.2	1044.3	7.0 6.0 5.0	
114	10.07	1058.77	0.27	1048.70			
			7.5	1051.3			
113	10.48	1068.61	0.64	1058.13			
			12.1	1056.5			
112			6.3	1062.3			
111+30			3.4	1065.2			
111			3.8	1064.8			
			7.63	1060.98			

June 1, 1927. Marks, D. Parks, Ransom Hassel¹⁴

FILL	AREA				CUBIC YARDS			
	RIGHT	EXCAVA	EMBANK.		EXCAVA.	EMBANK.		
X - N.E. cor	N. Headwall, Culvert W. of Chillicothe							
	10298	1029.4			1028.9	1028.9		
	9.5	9.9	10.1		10.4	10.4		
	140	50	5		50	100		
	14.0	13.4	12.0	7.7	7.4	8.1	7.9	8.2 8.5 10.0
	36.50	29	18.3	12	8	18	24	26 30 4.6
	Creek				shed			
	8.2	5.4	3.9	2.7	3.8	3.4	3.4	3.5 4.0 3.0 0.8 +11.0 +16.2
	33	26	20	16	15.5	11.5	0	8 9 11 17 37 42.5
	2.3	3.0	3.8	4.9	5.3	5.1	4.7	4.9 5.6 1.6 0.0 +4.0 +6.5
	33	26	18	15	11	9	0	4 8 13 18 22.5 33
					Fence			
	8.7	7.1	7.3	8.7	8.0	8.5		7.7 8.3 6.1 3.6 3.3
	50	22	12	10	8	0		5 7 10 22.5 2.5
	11.8	10.7	11.6	12.0	13.0	12.5	12.1	12.4 13.0 11.2 8.7
	45	27	12	11	9	7	0	7 8 14 22.5
	4.7	4.1	5.1	6.9	6.7	6.3		6.9 7.3 5.9 3.8 3.5
	50	24	11	8	6	0		8 9 10 16 21.6
	1.0	1.5	2.3	3.8	3.5	3.4		4.0 3.4 3.5
	50	20	10	8	6	0		10 12 21.0
	1.0	1.7	2.3	4.1	3.8	3.8		4.4 4.0
	50	24	11	8	6	0		7.0 12 20.8
	Spike in Tel. Pole 19.5' R. 107+94							

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
T.P.	6.05	1067.03		1060.98			X
110			5.3	1061.7			
109			6.3	1060.7			
	3.84	1067.92		1060.98			
108			4.5	1060.3			
	Good site for Culvert						
	4.07	1065.05		1060.98			
107			4.6	1060.4			
106+60			4.3	1060.7			
106			4.9	1060.2			
	4.88	1063.16	6.77	1058.28			
105			3.5	1059.7			
	3.68	1061.96		1058.28			
104			5.3	1058.7	1056.06		
	1.78	1060.06		1058.28			
103			6.1	1053.9			
	5.01	1056.74	8.33	1051.73	1051.49		
102			5.2	1051.5			

FILL	AREA		CUBIC YARDS	
	RIGHT	EXCAVA	EMBANK.	EMBANK.
1.4 30	1.5 22.5	2.6 17	4.4 13	4.9 10
5.3 12	5.0 14	4.0 21		
6.0 30	6.3 22.5	6.9 9	7.3 8	6.5 5
6.7 11	7.3 13	7.3 23	8.2 30	11.6 100
3.4 30	3.9 22.5	4.8 10	5.2 8	4.6 5
4.5 11	4.8 14	5.4 21	5.0 30	6.0 100
			10.5 160	13.0 180
1.8 30	2.3 22.5	4.1 11	5.4 8	5.7 5
4.6 10	4.9 12	5.4 14	4.8 22	4.1 30
0.5 29	1.2 22	2.4 17	4.1 12	5.5 9
4.9 9	4.3 11	4.4 13	4.9 21	3.7 30
2.5 29	2.9 22	2.9 17	2.9 12	2.9 9
3.1 30	3.4 22.5	5.0 12	6.0 9	5.0 6
4.8 9	5.4 11	6.3 14	5.7 13	4.9 20
5.9 30	5.9 30			
Tel. Pole R. 103+78				
1.7 30	2.7 22.5	3.5 16	5.1 12	3.8 7
3.5 10	4.3 11	5.1 19	4.5 30	5.9 30
1.7 30	2.0 22.5	2.3 17	4.5 13	6.4 10
5.1 8	5.4 10	5.1 12	4.2 20	5.3 30
2.0 30	2.2 22.5	2.7 18	6.4 10	8.0 9
6.5 6	6.1 7	6.6 9	7.1 11	5.1 23
4.3 30				
Temporary T.P. Stake				
4.8 30	4.8 22.5	5.4 18	6.6 11	5.5 8
5.2 6	5.7 6	6.2 9	5.7 11	4.2 20
4.6 30				

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
	2.50	1054.23		1051.73	1151.70		
101			4.2	1050.0			
			5.1	1049.1			
100+30	12" Corr. Pipe		5.1	1049.1			
	2.16	1053.89		1051.73	1051.70		
			3.2	1050.68	1050.15		
100			4.9	1049.0	1048.96		
	3.57	1054.25		1050.68			
99			4.2	1050.1			
	1.56	1052.24		1050.68			
98			4.6	1047.10			
			4.4	1047.80			
97+58.5	10" Corr. Pipe		4.4	1047.80			
	2.19	1052.87		1050.68			
97			4.6	1048.85			
	2.72	1052.40	3.19	1049.68			
96			2.8	1049.68			
95			1.7	1050.7			

FILL	RIGHT	AREA		CUBIC YARDS						
		EXCAVA	EMBANK.	EXCAVA.	EMBANK.					
3.5	3.9	4.3	4.8	5.4	4.6	4.2	4.9	5.4	5.1	5.6
30	22.5	18	12	11	8	8	10	13	30	
			1047.1				1046.4			
6.5	7.1	5.1		5.1	5.6	2.8	9.5	12.2		
22.5	10.2	8		8	8	10.2	50	100		
		F.L.				F.L.		ditch		
B.M. set, N. Root 24" Maple, 30' R, Sta. 99+00										
4.0	4.0	5.9	6.0	4.7	4.5	4.9	5.4	4.5	4.6	6.1
30	22.5	17	12	11	7	8	10	15	22.5	30
3.6	3.3	3.7	4.4	4.7	4.4	4.2	4.7	5.2	4.4	4.2
30	22.5	18	9	8	6	8	11	13	30	✓
3.0	3.9	5.3	4.6	4.6	4.8	5.2	6.0			
22.5	17	13	6	8	9	12	30			✓
		1045.8				1045.4				
5.3	6.4	4.3	4.4	4.8	6.8	2.5	9.3			
22.5	14.0	8	8	8	9.5	50	100			omit
		F.L.				F.L.				
3.8	5.4	4.8	4.6	5.0	5.5	5.1	5.3			✓
22.5	11	5	8	10	12	15	30			
T.P. Stake 1/2 ft. N. of Tel. Pole, R. 95+63										
10.3	11.5	1.3	0	-0.5	-1.0	-0.9	-1.5			
3.5	3.3	4.1	2.8	2.8	3.3	3.8	3.7	4.3		
22.5	15	10	5	8	11	13	14	30		
1.8	10.3	11.6	1.8	-0.2	-0.5	-0.9				
0.8	3.0	3.3	1.6	1.7	2.0	2.2	2.6			
22.5	15	11	6	8	11	13	30			

STA.	B. S.	H. I.	F. S.	ELEV.	GRADE	CUT OR	
						LEFT	C.
94	8.41	1058.09		1049.69			
				1052.99			
93+60.7	10.77	1060.45		1049.68			
			6.0	1054.4			
93			2.7	1057.7			
92	9.70	1070.15	0.00	1060.45			
			6.0	1064.2			
	11.85	1082.00	0.00	1070.15			
			4.15	1077.85			
91			10.3	1071.7			
90	11.88	1089.73		1077.85			
			10.7	1079.0			
89+50	9.29	1096.74	2.28	1087.45			
89			12.7	1084.0			
88			11.2	1085.2	1185.54		
87+33.5			11.1	1085.6			
				1085.64			

FILL	AREA		CUBIC YARDS		
	RIGHT	EXCAVA	EMBANK.	EXCAVA	EMBANK.
-0.7	0.7	-2.3	10.5	-0.4	3.7-5.1-5.7
5.8	5.8	7.4	4.6	5.1	5.5 8.8 10.6 11.2
22.5	20	18-15	8	8	13 20 32 36
10.12					1046.4
13.2	10.1	6.5	6.3	5.0 5.9 6.0	5.6 5.4 6.6 10.3 14.0
13.2			11	8 7 0	9 11 14.6
-7	-6.1	+0.4-4.8-0.1	-0.1	-0.1-0.4+0.3-3.1	-4.5-3.8
9.7	8.8	2.3	3.5 2.8 2.7	2.6 3.1 2.4 5.8	7.2 6.5
30	22.5	10	7 6 0	7 14 17 22	34 40
7.1	-0.2	5.7	+1.2+1.7-0.8-1.0	-0.5	-0.1-0.7-0.3+0.4+1.2+1.2
7.1	6.2	5.3	4.7 4.3 5.2 7.0 5.8	6.0	6.1 6.7 6.3 5.6 4.8 4.8
32	27	22.5	19 14 8 6.5 5.3	0	11 12.5 14 16.5 22-33
Nail, W. Side 30° Elm, 60' L 91+05					
3.7	5.6	6.1-1.3-0.6		-0.3-1.6+7.4	+7.3
6.6	4.7	4.2 11.6 10.9	10.3	10.6 11.9 2.9	3.0
40	22.5	16 8 5	0	9 11 23	40
June 2, 1927 Marks, D. Parks, R. Hassel					
+6.1	+7.4	+8.4-0.3-6.6-0.8	+2.5	-1.3-0.1+10.6	+10.4
4.6	3.1	2.5 11.0 12.3	11.5 10.7	11.2 12.0 10.8	0.1 0.3
40	22.5	19 7.5 6 4	5	10 12 13 28	40
6.9	5.6	5.2 12.0	15.6 15.1 14.5	15.3 15.8 12.0 2.3	3.2
40	22.5	19.5 13	5 4 0	9 10 17.5 28.5	40
13.8	4.5	+5.3-10.4-0.8-0.3	-0.3	-1.6+6.3+6.1	
8.9	8.2	7.4 12.3 13.5	13.0	12.7 13.0 14.3 6.4	6.6
30	22.5	14 7 5.5 4	0	9 11 24 30	
-0.7	-0.7	+0.5-0.4-0.7-0.3	-0.5	-1.0 0.1 +0.4	
10.5	10.5	10.7 11.6 11.9 11.5	11.2 11.7 12.2 11.3	10.8	
30	22.5	13 8.5 7 4	0	9 12 14 30	
					1082.1
10.5	10.5	11.6 11.4	11.1 11.4 14.0	12.0 12.3	
50	11	9 6	0 7 8	30 30	

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	G.
		1073.53 ✓					
58			4.5	1069.8			
	3.50	1074.45	2.58	1070.95 ✓			
57			3.5	1070.9			
56+50			2.7	1071.7			
56			3.2	1071.2			
55+44	± N. + S.	Road	7.8	1069.6	Caves Road		
55			4.3	1070.1			
54			4.6	1069.8			
53			4.6	1069.8			
52			5.8	1068.6			
51			7.8	1066.6			
	2.02	1068.73	7.74	1066.71			
50			3.0	1065.73			

FILL	AREA		CUBIC YARDS	
	RIGHT	EXCAVA	EMBANK.	EXCAVA.
+2.0	4.08	-07	-04	-05-07+09+06
2.5	3.7	5.2	4.9	4.5 5.0 5.2 4.1 3.9
22.5	12	8	6	0 10 13 16 30
spike, N. Side Tel. pole, 17.5' R. 57+90				
4.13	4	8		4.13 -06-09 -01 0
2.2	3.1	3.5		3.5 3.2 4.1 4.4 3.6 3.5
22.5	14	6		0 4 12 14 15 22.5
11.5	107	-06	-03	-07-09-03 114
1.7	2.5	3.8	3.5	3.2 3.9 4.1 3.5 2.8
22.5	9	7	5	0 11 13 15 22.5
1072.2	1072.6	1072.8	1072.1	1069.6 1069.0 1068.5 1068.0 1068.0 1068.1
2.2	1.8	1.6	2.3	4.8 5.4 5.9 6.4 6.4 6.3
150	100	65	50	0 50 100 150 200 250
on pipe				
1.9	7	-01	-07	-02
2.4	3.0	4.4	5.0	4.5 4.3
22.5	13	12	10	8 0
	0	-4	-08	-03
4.6	5.0	5.4	4.9	4.6
22.5	11	9	5	0
	0	-02	-06	-03-08
4.6	4.8	5.2	4.9	5.4
22.5	2	9	12	14 22.5
4.3	0	-09	-04	4.4 -05 -09-02 +0.3
22.5	10	8	5	0 3 11 13 15 22.5
4.3	6.0	6.8	6.1	5.8
22.5	9	7	4	0
4.3	5.7	6.2	6.7	6.0 5.7
22.5	4	11	13	15 22.5
4.2	1.2	8.7	8.2	7.8
22.5	10	8	5	0
	0.3	-02	-07-01+06	
7.5	8.0	8.5	7.9	7.2
22.5	5	12	14	15 22.5
-02-07	-1.2	-04		
3.3	3.7	4.2	3.4	3.0
22.5	9	7	5	0
	1.0	3	-11	-03+0.1
2.9	3.3	4.1	3.3	2.9
22.5	4	10	14	15 22.5

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	G.
49		1068.73	1	4.4	1064.3		
48				6.7	1062		
47				11.0	1057.7		
	1.02	1058.71		11.04	1057.69		
46				3.0	1055.7		
45				4.6	1054.1		
44				4.1	1054.6		
	6.58	1061.87		3.42	1055.29		
				3.57	1058.30		

FILL	AREA				CUBIC YARDS				
	RIGHT	EXCAVA	EMBANK.		EXCAVA.	EMBANK.			
	-8.7	-0.3	-1.6	-0.4	+0.2	-0.2	-1.2	+0.6	+0.9
	4.8	4.7	6.0	4.8	4.4	4.2	4.6	5.6	3.8
	22.5	9	7	5	0	3.5	10	13	15
	22.5	9	7	5	0	3.5	10	13	15
	4.9	4.1	3.4	-0.5			-0.8	-2.0	0.7
	6.3	6.2	9.1	7.2	6.7		7.5	8.7	6.0
	22.5	12	8	4.5	0		10	13	16
	22.5	12	8	4.5	0		10	13	16
	4.9	4.1	3.4	-0.5			-0.8	-2.0	0.7
	9.1	8.1	9.2	10.0	12.5	11.4	11.0	9.9	8.6
	30	18	14	11	7	4	0	10	12
	30	18	14	11	7	4	0	10	12
	-0.4	-0.1	-0.4	-0.6			-0.4	-0.7	-0.5
	3.9	3.1	3.4	3.6	3.0		3.4	3.7	3.5
	30	17	8	5	0		9	13	14
	30	17	8	5	0		9	13	14
	6.1	6.4	6.8				7.0	7.0	8.4
	200	100	8.0				12.3	100	200
	200	100	8.0				12.3	100	200
	-1.4	-1.3	+0.1				-0.4	-1.2	-0.5
	6.0	6.1	4.5	4.6			5.0	5.8	5.1
	22.5	9	4	0			9	12	15
	22.5	9	4	0			9	12	15
	4.5	4.1	0.8	-1	-0.4		-0.4	-1.3	-0.9
	2.6	3.1	4.9	5.1	4.5	4.1	4.5	5.4	5.0
	22.5	13	10	8	4	0	4	13.5	15
	22.5	13	10	8	4	0	4	13.5	15

W. Root 30" Ash 45' R, 40+10

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
43	1.39	1059.69 ✓		1058.30 ✓			
			3.6	1056.			
42			2.5	1057.1			
41+60			1.6	1058.			
41			2.9	1056.7			
40+25			3.3	1056.3			
40			4.2	1055.4			
39			9.9	1049.7			
38	1.87	1050.02 ✓	11.54	1041.15 ✓			
			3.9	1046.1			
37			6.9	1043.1			
36			10.4	1039.6			
35+55			12.9	1037.1			
35	0.63	1039.20	11.45	1038.57 ✓			
			6.9	1032.5	1032.3		
34	0.88	1028.61 ✓	11.47	1027.73 ✓			
			1.2	1024.4			

FILL	AREA						CUBIC YARDS	
	RIGHT	EXCAVA		EMBANK.		EXCAVA.	EMBANK.	
B. M. Right 40+10								
+02	-02	-07	+01					-05-12 -03-01
3.4	3.8	4.3	3.5	3.6	+0.1	3.5		4.1 4.8 3.9 3.7
22.5	10	8	4	0		4		11.5 15 17 22.5
+09	+04	-06	-04			+03		-01-07 +02+04
1.6	2.3	3.1	2.9	2.5		2.2		2.6 3.2 2.3 2.1
22.5	8.5	5	3	0		5		11 14.5 17 22.5
+03	-01	-05	-04			+04		-02-07 +01+07
2.6	3.0	3.4	3.3	2.9		2.5		3.1 3.6 2.8 2.1
22.5	6	5	3	0		5		12 14.5 16 22.5
-3	-1.4	-1.4						+2 -04 -9 -1 +0.4
4.5	4.8	5.6	4.6	4.2				4.0 4.6 5.1 4.3 3.8
22.5	13	6.5	4	0				2.5 9 11 13 22.5
+0.7	+0.5	+0.2	-07	-03				+02 -03 +1.0 +0.7 +3.1
7.2	7.4	7.7	6.6	6.2	9.9			7.7 12.2 13.9 6.7 6.8
30	24	8	6	4	0			3 10 12 19 22.5-30
						+0.3		-0.4 -1.2 +1.2 +1.5 +1.2
2.8	3.3	4.6	4.2	3.9		3.6		4.3 5.1 2.7 2.4 2.7
30	18	6	4	0		4		11 13 18 22.5 30
4.3	4.0	6.9	8.2	7.3	6.9	6.7		7.5 8.7 5.5 5.2 5.0
30	12.5	7	4	0		3		14.5 12 16 22.5 30
7.6	7.6	7.1	12.2	10.5	10.4			10.7 11.7 8.7 8.5 8.3
30	18	14	7	4	0			10 12.5 16 22.5 30
	0.0	9.0	7.0	6.9		6.6		7.9 6.9 6.5 1.7 1.7
30	18.5	8	5	0		8		11.5 12.5 15 21.5 30
1.5	0.7	4.5	4.2	4.0	4.2			5.3 7.4 2.1 1.9 1.6
30	15	11.6	0	4	10			13 14 18.5 22.5 30.0

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
		1034.85					
24			5.4	1029.4			
	1.54	1031.46		1029.92			
23			4.2	1027.2			
	1.47	1031.39		1029.92			
22			8.6	1022.7			
21					check		
	1.10	1021.21	11.28	1020.11			
21			5.8	1015.4			
	1.83	1011.09	11.95	1008.26			
20			4	1007.			
19			7.9	1003.1			
	4.35	1005.25	10.19	1000.90			
18			4.1	1001.1			
17			5.7	999.5			
16			5.3	999.9			
15	0.5, 3	5 1/2	2.8	1002.45	Stone Arch		
			5.25	1000.00			

FILL	AREA				CUBIC YARDS								
	RIGHT	EXCAVA	EMBANK.		EXCAVA.	EMBANK.							
2.8 24	3.6 10.5	6.2 7	5.6 4	5.4 8	5.2 4	5.7 9	6.2 11	5.6 13.5	5.3 22.5				
3.2 30	3.2 9	5.3 6	4.6 4	4.2 0		4.8 9	5.4 11	4.3 12	4.2 22.5	4.4 30			
6.7 30	6.0 16.5	9.0 12.5	10.6 10	9.1 7	8.6 8	8.6 6	8.8 9	9.9 16	4.7 22.5	4.5 30	4.0 1022.4		
		1021.6 9.8 30	1022.2 9.2 22.5							1022.7 8.7 18			
					1015.4								
					7.2 13	6.3 9	5.8 0		6.0 4.6	7.1 25			
	0.0 30	0.4 22.5	5.2 15	4.0 11	4.0 8	3.7 4	4.3 6.5	3.8 8	3.7 15	2.0 17	2.0 22.5	2.6 30	
	9.5 25	8.5 15	8.9 12	8.5 11	7.9 0						10.0 24		
	5.0 22.5	4.9 12	4.9 9	4.5 6	4.1					4.5 6	5.0 7	4.9 9.5	6.0 22.5
	6.2 22.5	6.1 13	6.1 11	5.9 7	5.7 0					5.7 8	6.0 10	6.0 12	6.6 22.5
	6.1 22.5	6.1 12	6.4 10	5.6 7	5.3 5								6.8 22.5
	990.8									991.2			
	11.4	9.7	8.6		2.8	2.5	6.9	14.1			10.1		
			5.8			13.3							11.6

Spike, F root W. Cherry, Left. 15+60

CWL VERT 5

STA.	B. S.	H. I.	F. S.	Elev. of Road		CUT OR LEFT C.
				Present	Proposed	
1+86.5	2.6	1004.7		1002.1	1004.1	F.L. Grade Grade Rod
15+05.3						
30+23.5	4.2	1020.5		1016.3	1018.4	F.L. Grade G.G. Rod
45+03	4.8	1058.9		1054.1	1055.1	
60+13.5	3.9	1072.5		1068.6	1069.6	

Apr. 10, 1928, W.C. Marks, D. Parks, C. Rand^{2nd}
Fair.

Elev.	North Side		South Side	
	RIGHT	AREA	EXCAVA	EMBANK.
1000.00	4'	16' → 16'	4' □	999.00
4.70		12" Corr. Pipe		5.70
Cut 2.0				Cut 2.0
1014.5	6.0	16' ← 16'	4' □	1015.3
Cut 2.0'		12" Corr. Pipe		5.2
				Cut 2.0'
1051.9	7.0	16' → 16'	4' □	1051.4
Cut 2.0'		15" corr. Pipe		7.5
				Cut 1.5'
1067.0	5.5	16' ← 16'	4' □	1067.2
Cut 1.0'		15" Corr. Pipe		5.3
				Cut 2.0

Apr. 11, 1928

W.C. Marks, D. Parks, C. Rand

30

Fair, Windy

N. Side

S. Side

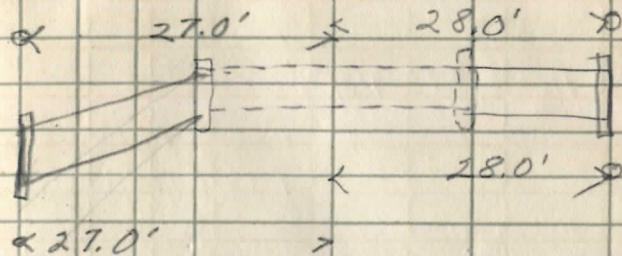
STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
87+23.5	2.0'	1087.6		1085.6	1087.1		

93+60.7

97+50.5	4.4	1052.2		1047.8	1050.0		
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100+30	4.9	1054.0		1049.1	1050.0		
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FILL	AREA	CUBIC YARDS	
		EXCAVA.	EMBANK.
RIGHT	EXCAVA. EMBANK.	EXCAVA.	EMBANK.
1083.0 4.6	16' 16' 15" Cor. Pipe	4' 4'	1083.5 4.1
Cut 1.0			Cut 2.0'



1046.5 5.7	16' 16' 12" Cor. Pipe	4' 4'	1046.0 6.2
Cut 1.5'			Cut 1.5'

1047.0 7.0	16' 16' 12" Cor. Pipe	4' 4'	1046.3 7.7
Cut 2.0'			Cut 0.0'

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
15+53.0							
B.M. 5.82	1005.82			1000.00			
			12.8	993.0			
			13.0	992.8			
			5.3	1000.5			
			13.8	992.0			
			7.57	992.25	992.25	13.57	6.0'
			7.07	992.75	992.75	13.07	6.0'

FILL	RIGHT	AREA		CUBIC YARDS		
		EXCAVA	EMBANK.	EXCAVA.	EMBANK.	
		Hub	30'	30'	Hub	16+00
			90°	90°		
			50'	50'		
			90°	90°		
			30'	30'		15+40.25
<p>Spike, E. Root, Wild Cherry, Left of 15+60 Creek Bed, 130' Left (North) " " 50' Left, (Sta 15+00) ⊕ Road 15+53 Creek Bed 100' Right (South) at Sta. 15+30 Top of stake, 50' Right, (South) Top of stake, 50' Left, (North)</p>						

Grades

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
B.M	4.47	1012.87		1008.90			
1				1005.00	7.87		
2				1004.00	8.87		
3				1004.50	8.37		
T.P.	19.33	1122.10	5.10	1007.77			
4				1008.00	12.10		
5				1013.00	7.10		
T.P.	10.45	1128.21	2.34	1019.26			
6				1018.00	10.21		
7				1023.00	5.21		
T.P.	13.41	1040.42	1.20	1027.01			
8				1028.00	12.42		
9				1033.00	7.42		
B.M			2+4	1037.98			
	5.12	1043.06		1137.99	Record		
10				1035.35	7.71		
11				1032.4	11.66		
12				1026.80	16.26		
T.P.	3.85	1032.78	14.13	1028.93			
13				1021.20	11.58		
14				1015.60	17.18		
T.P.	0.43	1016.91	16.30	1016.48			
T.P.	2.81	1009.92	15.80	1001.11			
B.M			4.61	999.31			
				1000.00	Record		

Rainy
June 7 1928 D. Parks, R. Hassel, C. Rand

FILL	AREA		CUBIC YARDS	
	RIGHT	EXCAVA	EMBANK.	EXCAVA. EMBANK.
Spike & Washer S.E. Side, 18' Maple, 12ft. rec. W of Sta				
2.04	C 1.8 33.0		7.82	C 0.1 24.5
12.01	F 3.1 20.0		11.90	F 3.0 19.5
10.02	F 1.7 22.0		7.53	C 0.8 25.0
Left Slope Stake Sta 4				
12.33	F 0.2 26.0		11.71	C 0.6 23.5
4.82	C 1.3 28.5		7.50	F 0.2 27.0
Slope Stake Rt Side Sta 6				
5.36	C 1.9 31.0		14.95	F 0.8 23.0
3.41	C 1.8 28.5		5.62	F 0.4 23.6
8.56	C 3.9 29.5		10.04	C 2.4 27.0
3.70	C 3.7 29.5		4.05	C 3.4 28.5
R.P. Nail N.W. Side, 15' Maple 40' Rt of Sta, 9+25				
3.41	C 4.3 31.0		6.42	C 1.3 26.0
6.87	C 3.8 30.5		8.20	C 2.5 22.0
10.77	C 5.5 30.5		12.01	C 4.3 35.0
Slope Stake Left of Sta 13				
3.85	C 7.7 37.0		10.40	C 1.2 27.0
7.73	C 9.5 38.0		14.65	C 2.5 27.0

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR		FILL	AREA		CUBIC YARDS	
						LEFT	G.		EXCAVA	EMBANK.	EXCAVA.	EMBANK.
		1138.57										
24				1032.00	2.57			0.86	$\frac{C2.2}{25.5}$		2.74	$\frac{F0.2}{22.5}$
	5.62	1036.25	1.94	1030.65								
25				1031.00	3.25			5.35	$\frac{F0.1}{22.5}$		6.13	$\frac{F0.9}{22.5}$
26				1032.00	4.25			5.19	$\frac{F0.9}{21.5}$		4.72	$\frac{F0.5}{22.5}$
	9.06	1040.59	4.72	1031.53								
27				1030.30	10.29			12.86	$\frac{F0.6}{21.0}$		4.60	$\frac{C5.7}{32.0}$
28				1025.90	14.69			15.80	$\frac{F1.1}{23.5}$		3.61	$\frac{C11.1}{40.5}$
	1.97	1026.89	16.47	1024.12								
29				1021.50	4.59			11.85	$\frac{F6.9}{24.0}$		6.44	$\frac{F1.9}{21.0}$
	4.56	1020.84	9.81	1016.28								
30				1018.48	2.36			5.88	$\frac{F3.5}{21.0}$		4.76	$\frac{F2.4}{20.0}$
31				1018.40	2.44			5.08	$\frac{F2.6}{19.0}$		4.28	$\frac{F1.8}{21.0}$
	9.30	1026.70	3.49	1017.35								
32				1019.70	7.05			9.35	$\frac{F2.4}{18.5}$		2.36	$\frac{F1.4}{22.5}$
33				1021.24	4.86			6.24	$\frac{F1.4}{17.5}$		6.00	$\frac{F1.1}{21.5}$
	16.15	1042.77	0.08	1026.12								
34				1027.00	15.77			15.25	$\frac{C0.5}{24.5}$		15.62	$\frac{C0.2}{25.0}$
35				1033.30	9.27			3.92	$\frac{C5.4}{32.0}$		4.91	$\frac{C4.4}{30.5}$
	9.84	1050.91	1.70	1041.02				7.18				
36				1032.38	11.53			9.18	$\frac{C2.4}{28.0}$		8.88	$\frac{C2.7}{27.0}$
37				1044.15	6.91			4.90	$\frac{C2.0}{26.0}$		5.67	$\frac{C1.2}{25.0}$
38				1048.00	2.91			3.54	$\frac{F0.1}{22.0}$		3.07	$\frac{F0.2}{24.0}$
	11.94	1061.08	1.77	1049.14								
39				1052.00	9.08			8.47	$\frac{C0.6}{23.0}$		8.00	$\frac{C1.1}{24.0}$

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
		1061.08					
40				1055.31		5.17	
B.M.		2.61	1058.47				
	2.61	1060.91		1058.30	Record		
41				1057.25		3.46	
	3.06	1060.24	3.73	1057.18			
42				1057.81		2.43	
43				1057.00		3.24	
	2.95	1058.91	4.28	1055.96			
44				1055.5		3.41	
45				1055.00		3.85	
	6.30	1061.77	3.44	1055.47			
46				1056.75		5.02	
	8.07	1067.16	2.68	1059.09			
47				1059.50		7.66	
48				1062.25		4.91	
T.P.	5.65	1070.14	2.67	1067.79			
49				1067.00		0.14	
50				1066.45		3.49	
51				1067.90		2.24	
52				1069.35		0.79	
T.P.	5.83	1074.66	1.31	1068.83			
53				1070.40		4.20	
54				1070.50		3.78	
55				1070.96		3.70	

FILL	AREA		CUBIC YARDS		
	RIGHT	EXCAVA	EMBANK.	EXCAVA.	EMBANK.
		$\frac{00.3}{22.0}$		$\frac{01.0}{24.5}$	
	5.47		4.79		
W. root of 30" Ash 45' Right, Sta 40+10					
		$\frac{00.1}{23.0}$		$\frac{00.5}{24.0}$	
	3.58		3.15		
		$\frac{00.4}{23.0}$		$\frac{0.0}{23.1}$	
	2.04		2.39		
		$\frac{00.4}{22.0}$		$\frac{0.9}{21.5}$	
	3.68		4.09		
Slope Stake Left Sta 44					
		$\frac{00.5}{24.5}$		$\frac{01.0}{21.5}$	
	2.95		4.70		
		$\frac{02.3}{21.5}$		$\frac{02.2}{22.5}$	
	6.14		6.05		
		$\frac{01.7}{22.0}$		$\frac{01.4}{22.0}$	
	6.71		6.37		
		$\frac{00.3}{24.0}$		$\frac{01.0}{24.0}$	
	7.33		6.63		
		$\frac{00.1}{23.5}$		$\frac{02.2}{26.5}$	
	4.89		2.67		
Slope Stake Rt. of Sta 48					
		$\frac{01.2}{21.5}$		$\frac{00.2}{24.0}$	
	6.35		4.92		
		$\frac{01.5}{21.5}$		$\frac{00.4}{22.0}$	
	4.83		4.29		
		$\frac{00.1}{23.0}$		$\frac{00.6}{21.0}$	
	2.14		2.79		
		$\frac{00.4}{21.5}$		$\frac{00.6}{22.5}$	
	1.14		1.34		
		$\frac{00.2}{23.0}$		$\frac{00.3}{22.5}$	
	4.44		4.51		
		$\frac{01.2}{21.5}$		$\frac{01.7}{21.0}$	
	4.97		5.51		
		$\frac{01.4}{25.0}$		$\frac{00.9}{22.0}$	
	2.32		3.70		

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
		1074.66					
T.P.	8.54	1076.07	1.15	1073.51			
56				1071.04	5.01		
57				1071.12	4.93		
58				1070.00	6.05		
59				1069.87	6.68		
	4.70	1074.59	6.16	1069.89			
60				1069.50	5.09		
61				1070.50	4.09		
62				1070.50	4.09		
63				1071.75	3.34		
64				1072.50	2.09		
T.P.	4.86	1077.28	2.17	1072.42			
B.M.		2.56	1074.92				
				1074.70	RECORD		
	5.35	1080.11		1074.76			
65				1074.19	5.92		
66				1074.25	3.26		
T.P.	7.43	1082.56	2.92	1077.13			
67				1078.19	5.87		
68				1081.50	3.06		
	5.83	1087.70	2.69	1081.29			
69				1084.50	3.20		
	6.09	1090.11	2.13	1125.52			

FILL	AREA		CUBIC YARDS	
	RIGHT	EXCAVA	EMBANK.	EMBANK.
		0.17		0.8
3.27		25.5	4.24	24.0
3.62		1.3	4.93	2.0
4.86		25.5		23.0
8.16		1.2	6.27	2.0
		24.5		2.0
		F1.5	7.95	2.0
		21.0		
		F1.7		F1.5
6.81		20.5	6.60	20.0
5.95		F1.7	5.23	F1.8
4.23		22.0		21.5
3.34		F0.2	3.67	0.4
		22.5		22.5
1.94		0.0	2.47	0.9
		22.5		25.5
		0.2	1.73	0.4
		23.0		23.0
SPIKE, S. side, 2 1/4" Hickory 26 L, ST 9 67 1/2.				
Fair Work				
June 27, 1928, P. Parks; C. Pond, R. Hooper				
		10.0		F0.1
5.89		23.0	5.99	23.0
1.51		0.2	3.34	0.3
		26.0		23.0
		C2.7		F0.4
3.12		26.5	6.31	2.0
1.66		C1.4	3.12	F0.5
		24.0		2.0
		C1.4		0.0
1.82		24.5	2.20	24.5

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
		1091.61					
70				1086.60		5.21	
	6.08	1173.94	4.20	1087.41			
71				1088.70		4.79	
	5.82	1025.31	4.00	1089.49			
72				1090.80		4.51	
73				1092.00		3.31	
	5.64	1026.78	4.17	1091.14			
74				1093.20		3.52	
75				1094.38		2.40	
	7.77	1101.02	3.63	1093.25			
76				1095.20		5.62	
77				1096.24		4.78	
78				1096.90		4.12	
79				1097.38		3.64	
80				1097.70		3.32	
	5.24	1102.12	4.14	1096.38			
81				1097.49		4.63	
82				1096.25		5.87	
B.M.			2.73	1099.39			
				1099.20		record	

FILL	RIGHT	AREA		CUBIC YARDS	
		EXCAVA	EMBANK.	EXCAVA.	EMBANK.
	3.95	$\frac{C1.7}{24.0}$		3.23	$\frac{C1.3}{25.0}$
	4.14	$\frac{C0.6}{24.0}$		3.79	$\frac{C1.0}{23.0}$
	5.75	$\frac{F1.2}{23.0}$		4.15	$\frac{C0.4}{22.0}$
	3.72	$\frac{F0.5}{22.5}$		4.41	$\frac{F1.1}{21.0}$
	4.86	$\frac{F1.3}{21.5}$		5.07	$\frac{F1.5}{21.0}$
	2.66	$\frac{F0.3}{22.0}$		3.44	$\frac{F1.0}{22.0}$
	5.70	$\frac{F0.3}{22.0}$		6.10	$\frac{F2.5}{22.0}$
	1.76	$\frac{0.0}{25.0}$		5.07	$\frac{F2.3}{22.0}$
	3.72	$\frac{C0.4}{22.5}$		4.44	$\frac{F0.3}{22.5}$
	5.73	$\frac{F0.1}{22.0}$		4.64	$\frac{F1.0}{22.0}$
	4.22	$\frac{F1.0}{21.0}$		4.20	$\frac{F0.9}{22.0}$
	4.65	$\frac{0.0}{22.0}$		4.87	$\frac{F0.2}{23.5}$
	3.58	$\frac{C2.3}{24.0}$		3.85	$\frac{C2.0}{23.0}$

R.P.Nail, N. Side, 30" Asy, 33' Right, 5784 + 30

STA	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
B.M.	2.49	1101.79		1099.30			
83				1094.50	7.29		
84				1090.25	9.04		
	4.20	1194.74	11.25	1090.54			
85				1091.00	3.74		
86				1089.25	5.49		
87				1087.50	7.24		
88				1085.75	8.99		
	1.04	1095.71	0.07	1094.67			
89				1088.02	12.69		
90				1078.33	17.38		
	1.40	1188.32	8.79	1086.92			
91				1078.17	15.65		
B.M.		10.39	1077.93				
	10.39	1082.24		1077.85	RECORD		
	1.82	1078.17	11.89	1076.35			
	1.32	1067.62	2.37	1065.80			
92				1067.00	0.62		
93				1061.33	4.29		
	5.61	1158.05	15.08	1052.54			
94				1055.67	2.48		
95				1051.42	6.73		
	4.47	1055.60	7.02	1054.13			
96				1050.00	5.16		

FILL	AREA		CUBIC YARDS		
	RIGHT	EXCAVA	EMBANK.	EXCAVA.	EMBANK.
FILL WIDTH June 28/1902. P. Banks, C. Rand, R. Nassar					
R.P. Nail W. side	30" Right	33' Right	Sta 87+33		
6.93	C1.7 23.5	6.18	C1.1 24.5		
10.41	F1.6 20.5	10.30	F1.2 21.5		
6.82	F3.1 19.5	4.20	F0.6 22.0		
3.06	C2.4 25.0	1.77	C3.7 29.0		
11.18	F3.9 20.0	8.51	F1.3 21.5		
8.26	C0.7 23.0	8.25	C0.1 22.5		
7.24	C5.5 28.5	5.59	C7.1 35.0		
9.16	C8.2 30.0	5.82	C11.6 40.0		
11.15	C4.6 27.5	8.47	C1.2 33.0		
Nail W. side 30" E 1/4 60' x Sta 91+05					
18.41	F1.2 16.5	2.34	F1.7 20.0		
14.51	F16.2 29.0	11.58	F5.3 20.0		
3.26	F1.7 28.0	7.68	F5.2 25.0		
4.55	C2.2 21.5	6.02	C0.7 20.5		
3.69	C1.9 21.5	4.98	C0.6 21.0		

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
97	1055.60				1050.00	5.00	
98	6.14	1074.96	1048.82		1050.00	4.96	
99					1050.00	4.96	
		2.34		1152.12			
B.M.	4.51	1082.30		1077.85			
	1.02	1170.72	12.16	1069.70			
92					1067.00	3.72	
	4.03	1061.27	13.48	1057.24			
93					1061.33	4.06	
	3.69	1056.26	8.70	1052.57			
94					1055.17	0.59	
95					1051.42	4.84	
	3.91	1053.47	6.70	1049.56			
96					1050.00	3.47	
97					1050.00	3.47	
	4.38	1052.55	0.00	1048.17			
98					1050.00	2.85	
99					1050.00	2.85	
		2.20		1050.65			
				1050.68			TECOT

FILL	AREA	CUBIC YARDS	
		EXCAVA	EMBANK.
4.51	CL.1 21.0	5.47	50.1 20.5
3.88	CO.1 21.0	6.44	FI.2 20.0
1.61	C3.4 24.0	2.75	CP.3 24.0
Showers Windy			
June 29, 1928 D. Parks, C. Pond, K. Hasse			
Nail W side 30" F177 60' - STA 91+05			
5.02	FI.3 16.0	5.48	FI.8 20.0
10.26	FI.3 29.0	5.79	FI.4 20.0
3.92	FI.3 22.0	7.74	FI.2 25.0
4.60	CO.2 21.5	6.88	FI.3 20.5
3.52	FO.1 21.5	4.81	FI.3 21.0
4.33	FO.9 21.8	5.30	FI.3 20.5
3.75	FO.9 21.0	5.98	FI.1 20.0
1.48	CH.4 24.0	2.60	CO.3 24.0
N FOOT, RAW Maple 30' Right, STA 99+00			

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
	3,19	1053,87		1150,68			
100					1030,00	3,87	
101					1150,75	8,12	
	8,12	1052,94	3,05	1050,82			
102					1052,00	5,94	
103					1033,73	3,21	
	6,87	1063,25	2,55	1056,39			
104					1057,92	5,34	
105					1059,57	5,69	
	6,92	1066,85	3,33	1059,93			
106					1060,62	6,17	
107					1061,85	5,60	
	4,92	1065,25	6,52	1060,33			
108					1061,55	3,70	
109					1061,95	5,30	
	4,55	1068,17	1,63	1063,62			
110					1063,10	5,07	
111	4,94	1069,68	3,43	1064,74			
111					1064,50	5,18	
112					1064,50	7,18	
113					1057,00	12,68	
	2,52	1053,94	4,21	1055,42			
114					1057,00	6,99	
115					1044,50	13,49	

FILL	AREA		CUBIC YARDS		
	RIGHT	EXCAVA	EMBANK.	EXCAVA.	EMBANK.
	3,76	$\frac{F0,1}{22,5}$		4,46	$\frac{F0,6}{22,0}$
	3,85	$\frac{F0,2}{22,5}$		5,04	$\frac{F1,9}{21,0}$
	6,85	$\frac{F0,7}{20,5}$		6,34	$\frac{F0,4}{23,0}$
	0,89	$\frac{C0,8}{26,5}$		8,30	$\frac{C0,9}{25,0}$
	2,82	$\frac{C2,5}{29,5}$		6,11	$\frac{F0,8}{26,0}$
	2,13	$\frac{C1,6}{25,0}$		5,02	$\frac{F1,3}{22,5}$
	4,62	$\frac{C1,6}{25,5}$		4,70	$\frac{F0,5}{23,0}$
	3,58	$\frac{C0,9}{26,0}$		5,84	$\frac{F0,2}{23,0}$
	4,15	$\frac{F0,5}{22,5}$		5,35	$\frac{F1,7}{21,0}$
	4,15	$\frac{F0,2}{21,5}$		5,22	$\frac{F1,9}{18,5}$
	2,30	$\frac{C2,8}{26,5}$		5,56	$\frac{F0,5}{21,5}$
	2,04	$\frac{C3,1}{26,0}$		4,94	$\frac{C0,2}{19,0}$
	4,80	$\frac{C2,4}{26,5}$		4,34	$\frac{C2,8}{22,5}$
	11,95	$\frac{C0,7}{24,5}$		10,16	$\frac{C2,5}{21,0}$
	6,20	$\frac{C0,8}{24,5}$		2,54	$\frac{C3,6}{22,0}$
	11,81	$\frac{C1,7}{25,0}$		4,11	$\frac{C9,4}{26,0}$

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
		1049.40					
94				1055.17		13.73	
	2.03	1055.13	16.30	1053.10			
95				1051.42		3.71	
B.M.			4.43	1050.70			
				1054.63		record	

FILL	AREA		CUBIC YARDS	
	RIGHT	EXCAVA	EMBANK.	EMBANK.
		14.23	1055.17	
		4.47	1050.66	
N. root 24" Maple 30' P. Sta 99+00				

Finish Grades

STA.	B. S.	H. I.	F. S.	ELEV.	GRADE	CUT OR	
						LEFT	C.
B.M	9.73	1046.93		1031.80			Grade Req
116+50				1033.00		7.93	
116+80				1037.00		3.93	
B.M.	1.98	1176.74		1074.76			
64				1072.50		4.24	
63				1071.25		5.49	
62				1070.50		6.24	
61				1070.50		6.24	
60				1069.50		7.24	
59				1069.37		7.37	
T.P.	4.53	1075.645	63	1071.11			
58				1070.00		5.64	
57				1071.12		4.52	
56				1071.04		4.60	
T.P.		2.04					

FILL RIGHT	AREA		CUBIC YARDS	
	EXCAVA	EMBANK.	EXCAVA.	EMBANK.
Fair August 9, 1928				
D. Parks, C. Rand X-N.E. Coty, N. Head-wall Culvert W. of Chillicothe Rd.				
Fair August, 13, 1928				
D. Parks, C. Rand, R. Hassel				
Spike S. side	24" Hickory 26' left, Sta. 64+53			
Profile	4.55	1073.19		
	6.47	1070.22		
	7.26	1067.48		
	7.71	1069.03		
	8.03	1068.71		
	7.77	1068.97		
	6.30	1069.54		
	5.01	1070.63		
	5.09	1070.55		
Large Stone left of Sta. 55+85				

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR		FILL	AREA		CUBIC YARDS	
						LEFT	C.		RIGHT	EXCAVA	EMBANK.	EXCAVA.
B.M	5.84	1080.60		1074.7								
65				1074.19		6.41			6.72		1073.88	
66				1076.25		4.35		4.81		1076.39		
67				1078.69		1.91		2.27		1078.33		
T.P.	8.68	1087.75	1.53	1079.07								
68				1081.50		6.25		6.73		1081.02		
69				1084.50		3.25		3.85		1083.90		
70				1086.60		1.15		1.29		1086.46		
	8.86	1095.47	1.14	1086.61								
71				1088.70		6.77		7.04		1088.43		
72				1090.80		4.67		5.38		1090.09		
73				1092.00		3.47		4.46		1091.01		
74				1093.80		2.27		3.48		1091.99		
75				1094.38		1.09		2.26		1093.21		
76				1095.40		0.07		1.25		1094.22		

0.03

Spike S side 24" Hickory 26' left Sta 69+53
~~Ames Rod~~ subGrade
~~24" Hickory~~ Sub-Grade

Slope hub right of Sta 72.

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	G.
		1159.86					
T.P.	7.03	1064.15	2.74	1057.12			
105				1057.57	7.58		
106				1060.13	3.47		
107				1061.25	2.90		
108				1061.55	2.60		
109				1061.75	2.20		
T.P.	2.49	1066.50	0.14	1067.01			
110				1063.10	3.40		
111				1064.50	2.00		
111+50				1064.00	2.50		
112				1062.50	4.00		
112+50				1060.00	6.50		
113				1057.00	9.50		
T.P.	0.62	1054.59	12.59	1053.91			
114				1051.00	3.53		
115				1044.50	10.03		
T.P.	0.44	1042.18	12.79	1041.74			
116				1037.00	5.18		
116+50				1033.00	9.12		
B.M.		1096		1031.22			
				1031.20	Record		

FILL	AREA	CUBIC YARDS	
		EXCAVA.	EMBANK.

Slope Hub Right Sta 104

5.0

4.3

3.7

3.1

2.5

Grade stake RT, Sta 110

3.8

2.5

3.3

4.9

7.0

9.8

3.7

11.5

X = N.E. Cor. N. Head-wall culvert w. Chippicotte road

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	G.
B.M.	3.91	1062.21		1058.30			
40				1055.31		6.90	
41				1057.28		4.96	
42				1057.81		4.40	
43				1057.00		5.21	
44				1055.5		6.71	
45				1055.06		7.15	
T.P.	12.01	1067.157.07		1055.14			
46				1056.75		10.40	
47				1059.50		7.65	
48				1062.25		4.90	
49				1065.00		2.15	
50				1066.45		0.70	
T.P.	8.58	1074.59	1.14	1066.01			
51				1067.90		6.69	
52				1069.35		5.24	
53				1072.46		4.13	
54				1070.88		3.71	
55				1070.96		3.63	
T.P.			1.02	1073.67			

FILL RIGHT	AREA		CUBIC YARDS	
	EXCAVA	EMBANK.	EXCAVA.	EMBANK.
Fair W th				
Aug. 23, 1928				
D. Parks, C. Rand, R. Hassel				
W. root of 30" Ash				
45' Right Sta. 40+10				
Red sub grade at top	7.5	1054.71		
	5.5	1056.71		
	5.00	1157.21		
	6.1	1056.11		
	7.8	1054.41		
	7.9	1054.31		
	11.70	1055.75		
	8.9	1058.25		
	5.4	1061.75		
	2.9	1064.25		
	1.5	1065.65		
	7.7	1066.89		
	6.0	1068.59		
	4.7	1069.89		
	4.7	1069.89		
	4.4	1070.19		
Large Stone	25"	left Sta.	55+80	

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	G.
							Graded
B.M.	1.90	1060.20		1058.30			
T.P.	1.31	1048.83	12.28	1047.52			
36					1039.38	9.15	
	4.25	1043.46	9.22	1039.21			
35					1033.50	9.92	
B.M.	1.12	1054.06		1057.94			
18					1035.35	6.71	
B.M.	4.07	1042.01		1037.94			
10					1035.35	6.66	
11					1032.4	9.61	
	2.11	1032.60	11.52	1030.49			
12					1026.80	5.80	
13					1021.20	11.40	
	0.76	1021.96	11.40	1021.20			
14					1015.60	6.36	
	1.24	1011.12	12.08	1009.88			
15					1010.00	11.12	
16					1004.40	6.72	
B.M.				9.60	1001.52		
17					1000.73	10.39	

Slope line Stakes
 Fair. W. H. D. Y.
 Aug. 28, 1928 D. Parks, C. Rand, B. Hassel
 W. root 30" Ash 45' Right, Sta. 10+10

Check grade stakes & slope stakes
 Sept. 1, 1928 D. Parks, C. Rand

Grade Stake Rt Sta. 13

12.32 Fb16
 N.E. Cor., N. Headwall, B.M. Set
 84" Cor. Iron Culvert

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	G.
E. M.	1.59	1059.89		1058.30			
				1052.00			
				52.00		7.89	
				1048.60		11.89	
T.P.	1.79	1049.79	11.89	1048.00			
				1044.00		5.79	
				1039.38		10.41	
T.P.	2.07	1039.42	12.41	1037.35			
				1033.50		5.92	
				1027.00		12.42	
		0.23	1027.23	12.42	1027.00		
				1021.84		5.39	
				1019.70		7.53	
				1018.40		8.83	
				1018.48		8.75	
				1021.50		5.73	check
T.P.			9.72	1017.51			

FILL	AREA		CUBIC YARDS	
	RIGHT	EXCAVA	EMBANK.	EMBANK.
Fair Warth sept. 5, 1928		Sub grade		R. Hasse?
		Rad	Grade	D. Parks, E. Pond, R. Hasse
W. cut 30" Ash		45	RT. Sta 40+10	
		8.9		
		12.7		
		Grade stake Lt Sta 38		
		6.2		
		14.0		
		6.5		
		13.3		
		Grade stakes Rt Sta 37		
		5.9		
		8.3		
		9.8		
		9.6		
		X-S, E Cor. N. Headwall	Sta 30+23.5	

STA.	B. S.	H. I.	F. S.	ELEV.	GRADE	CUT OR	
						LEFT	C.
		1024.62					
30				1018.48	61.4		
t.P.			7.01	1017.61			
			1017.51				
9/30/52							
2.03	1103.43			1101.4	Top N. Hd wall		
			0.3	03.1	± 50 ft E of P.C.		
			7.9	1075.5	± 10' E of P.C. creek		
			6.0	97.4	P.C.		
			3.3	1100.1	90' W of P.C.		
9.62	1111.02			1101.4	117'		
			4.5	06.5	117' W of P.C.		
			4.8	06.2	160' W of P.C. =		

99.66 bottom
9/30/52

SEE FB 173
PAGE 79

See further notes
173 pg 79 et seq
BK

FILL RIGHT	AREA		CUBIC YARDS	
	EXCAVA	EMBANK.	EXCAVA.	EMBANK.
		6.7		
X S.E. Cor. N. Headwall 12" corr. pipe Culvert 30+23.5				
Fairmount (D) Sta 62+?				
the of steep slope				
top steeper slope & brush				

LEVELS FOR CULVT

60+13.5

STA.	B. S.	I.S. H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
B.M	4.17	62.47		1058.30	W root Ash	40+10	
T.P.	11.66	66.72	7.41	55.06			
"	8.78	75.07	0.43	66.29			
"	3.18	74.15	4.10	70.97			
			4.8	69.35	± Ed ± culvt		
			4.37		N.W & N. Hdwl		
			7.67	66.48	N. FL		
			7.36	66.79	S. FL		
			4.10		S Hdwl		
			8.19	65.96	Top of tile (Field drain)		
			8.2		100' N of N hdwl		
			8.6		200 " " " "		
			8.9	65.25	300		
T.P. ^{sk}			7.75	66.40			
T.P. Ed			3.62	70.53			
T.P. ^{sk}	3.31	69.71		66.40			
			5.8	63.9	400'	" " " "	
			6.5		500'	" " " "	
			7.7		600'	" " " "	
T.P. ^{Ed}	6.19	76.72		70.53			
B.M Set			2.79	73.93			

5-29-46 Pomeroy
Thrasher
Bell

FILL	AREA		CUBIC YARDS	
	RIGHT	EXCAVA	EMBANK.	EMBANK.

Note: End of tile ± 3' S of S headwall 4" round tile

Culvt = 15" x 32" Corr. I. P.
Bottom half rusted

See FB 173 Pg 25
for 1956 notes

76.72
74.76
1.96

Spk 5 root

27" Hick Sta 64+53 26' H

1241
392
163

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	G.
		1036.88					
5+00							
5+50							
6+00							
T.P.			7.15	79.73	Hub	6+12 on 75'	
6/19/50							
T.P.				65.10			
	7.40	172.50					
5+00							
5+50							
5+98							
6+00							
T.P.	3.75	63.75	12.50	60.00			
6+50							
T.P.	1.40	52.06	13.09	50.66			
6+50							
T.P.			1241	39.65	top of c	6+50	
T.P.	11.00	71.00		60.00			
BM			322	1067.78			

Hor Lt

Sort

FILL	AREA		CUBIC YARDS	
	RIGHT	EXCAVA	EMBANK.	EMBANK.
N M LT.			34.5	30.8
			31.7	30.7
			31.1	
			2.4	6.1
			5.2	6.2
			5.8	5.8
			4.9	5.8
			6.8	7.6
			8.3	8.3
			30.0	31.3
			6.9	5.6
			6.7	6.7
			7.5	8.5
			8.3	8.3
			29.5	30.6
			7.4	6.3
			7.1	7.1
			8.2	9.0
			9.3	9.3
top 4+50 ±				
	67.2	67.7	66.0	61.8
LEVEL	5.3	4.8	6.5	10.7
30' MARK	5.2	1.5		12
	69.2	67.6	66.5	60.7
LEVEL	3.3	4.9	6.0	11.8
25' MARK	3.5	1.5		14
	(5+88)	6.9	65.6	
	68.8	66.0		
	4.2	6.5	14.0	58.5
	6.0	1.6		
	60.8	59.3		
GRAD. V ²	2.45	4.4		
N 14	6.0	4.5		
			36.7	
			15.33	
+ 30' NW of ± S/s 6+0 Spk Sroot 18" Wild Ch				

Herb 6/20/50
Tom

ck back

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	G.
BM	1.79	39.76		1037.47			
T.P.	4.26	33.33	10.19	29.07			
T.P.	2.26	33.72	1.87	31.06			
BM			4.12	1029.60 (1029.59)			
8/21/50 Herb - Art							
Profile $\frac{1}{4}$							
BM				1037.67			
	7.75	1045.22					
17+00			6.96	38.26			
18+00			5.75	39.47			
19+00			3.88	41.34			
20+00			1.24	43.98			
T.P.	11.45	1055.44	1.23	1043.99			
21+00			8.15	47.29			
22+00				51.86			
T.P.	12.53	1065.97	2.00	1053.44			
23+00				57.88			
23+10							

FILL RIGHT AREA EXCAVA EMBANK. CUBIC YARDS EXCAVA. EMBANK.

NE 4 E end conc. hdwl

NE 4 E end hdwl NE quad 306 of CH 16

NE 4 E end conc. hdwl South side road

N 49.9 47.0 E 46.8 44.1 49.7 S 50.8
 5.54 easy 8.38 8.15 8.62 11.25 5.75 4.64 easy
 35.0 up drive 11.0 berm DITCH 11.0 17.0 25.0 31.0 up out

54.3 54.0 51.2 51.5 51.3 47.5 52.5 53.6
 1.18 1.36 4.28 3.92 4.28 7.85 2.86 1.92 easy
 30.0 20.0 12.0 18.5 3.58 10.0 15.0 23.5 30.0 up
 DITCH berm berm DITCH

47.2 41.1 57.3 57.2 57.2 57.8 57.7 57.3 56.0 57.4 56.8 55.9
 4.80 4.97 8.72 8.52 8.50 8.21 8.34 8.74 9.95 5.61 9.21 10.86
 2.0 25.0 15.0 13.0 11.0 7.0 8.09 10.0 13.0 15.0 18.0 24.0 30.0
 Ditch Ditch

47.0
Bank
14.0

♀

STA.	P. S.	D. S.	N. I.	F. S.	ELEV.	GRADE	CUT OR	
							LEFT	C.
			1065.97					
23+90								
24+00					1065.29			
T.P.	6.02	1070.98	1.01		1064.96			
24+50					67.34			
25+00					65.65			
25+90					60.96			
T.P.	7.22	1067.35	10.85		1060.13			
26+15					1060.20			
NEW B.M. 5C7 1952 26+71 culvert Sta.		± 60 S of Culvert			1055.87	5 ft N side most SE 1/4 WILLOW		
					59.35			
27+00					60.07			

FILL RIGHT	AREA		CUBIC YARDS	
	EXCAVA	EMBANK.	EXCAVA.	EMBANK.
N		♀		63.5
			2.92	-17.0
	66.2	66	65.4	64.9
	-0.25	0.00	0.62	1.05
	30.0	20.0	13.0	10.0
				0.68
				0.86
				1.32
				1.93
				1.10
				13.5
				-0.50
				30.0
				Ditch
				67.9
				67.4
				67.4
				66.9
				67.5
				70.3
				Level
				3.13
				3.61
				3.59
				3.58
				4.06
				35.3
				0.72
				Ditch
				67.5
				66.8
				65.4
				65.4
				65.4
				65.4
				65.4
				66.8
				68.4
				71.0
				72.1
				3.51
				4.20
				5.77
				5.60
				5.28
				5.42
				5.57
				4.23
				2.55
				0.0
				-1.1
				28.5
				21.0
				15.0
				13.0
				5.28
				7.0
				9.0
				12.0
				16.0
				17.0
				30.0
				Ditch
				57.1
				60.1
				60.8
				61.0
				60.7
				61.9
				62.2
				64.5
				73.7
				13.86
				10.65
				10.21
				9.97
				9.23
				10.26
				9.14
				8.05
				5.98
				-2.17
				30.0
				17.0
				16.0
				12.0
				26.0
				Ditch
				59.9
				59.3
				59.2
				60.1
				59.5
				60.9
				63.0
				11.5
				8.10
				7.58
				7.15
				7.30
				7.90
				8.55
				4.38
				30.0
				Ditch
				50.7
				57.7
				58.7
				50.6
				16.68
				9.68
				8.65
				16.75
				Flowline
				outlet
				Top
				headwall
				8.0
				Top
				headwall
				Flowline
				inlet
				56.2
				59.0
				57.2
				59.4
				59.8
				10.21
				8.62
				7.60
				7.28
				7.75
				12.29
				12.30
				30.0
				Ditch

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	C.
		1153.76					
25	56+0			42.6			
	T.P.	2.47	1143.97	12.26	1141.50		
					1135.6		
	T.T.P.	1.53	1132.54	12.96	1131.01		
					26.2		
	T.P.	2.53	1124.73	10.34	1122.20		
25	59+0			18.4			
	T.P.	0.39	1112.22	12.90	1111.83		
					11.5		
26	61			1109.2			

9/30/57
Pg. 53 = part location profile

121
Clvt

FILL	RIGHT	AREA		CUBIC YARDS				
		EXCAVA	EMBANK.	EXCAVA.	EMBANK.			
	45.2	46.4	41.8	1142.8	42.2	41.8	41.2	43.4
	2.9	7.4	12.0	11.0	11.5	12.0	12.7	10.7
	4.0	19.0	10.8	8.0	17.0	23.0	26.0	30.0
	44.5	43.0	33.2	31.6	35.2	35.8	35.1	34.2
	easy up	1.0	10.7	7.4	8.8	8.3	8.2	8.9
	9.5	29.0	11.0	6.0	8.4	6.0	14.0	21.5
	40							
	25.5	24.2	25.2	11.97	26.2	25.8	25.2	25.8
	7.0	8.3	7.2	6.1	5.9	6.7	7.5	6.7
	30.0	21.5	26.5	12.0	7.0	6.3	7.0	16.0
	15.1							
	48.0							
	35.6							
	33.5	17.2	17.3	17.8	18.0	11.84	17.8	17.6
	level 1.2	6.9	7.4	6.9	2.7	6.3	6.9	7.1
	34	27	24	21.5	16	8	10	11
	11.3	09.2	08.0	11.2	11.4	111.6	10.5	09.3
	0.9	2.6	3.2	1.1	0.8	0.7	0.6	1.7
	35	19	17	11	3	7	19	29
	1097.2	1092.3	1106.6	07.5	06.1	04.8	03.7	1099.9
	+15.0	12.9	5.6	5.0	4.7	6.1	7.4	8.5
	+level	33	27	9	11	28	42	46
	1100.8	1095.0	1107.0	1095.2	1101.4			
	11.4	17.2	5.2	17.6	108			
	Top of flow			flow	flow			Top
	hd wall			line	line			hd wall

23.50
19.51
40

STA.	CORRECTION		F. S.	ELEV.	GRADE	CUT OR	
	B. S.	H. I.				LEFT	R.
		1112.22					
6240				1109.0			
T.D	10.73	1122.50	0.45	1111.77			
63				16.9			
T.P.	10.48	1132.62	0.36	1122.14			
64				28.3			
T.P.	11.00	1143.60	0.02	1132.60			
T.P.	8.45	1151.04	1.01	1142.59			
65				41.1			
+32	Cuyahoga Trail						
T.P.	9.27	1160.23	0.08	1150.96			
66				52.7			
T.P.	9.00	1168.73	0.50	1159.73			
67				60.9			
68				63.5			

N = trav &
E

FILL	AREA		CUBIC YARDS	
	RIGHT	EXCAVA	EMBANK.	EXCAVA. EMBANK.
1101 ⁰	02 ⁵	07.5	1108.9	07.9 08 ¹ 07.6 06.1 1106 ⁵
1112	9.7	4.6	3.3	4.3 7.1 4.6 6.1 7.6
70.0	37.5	13.5	3.2	7.0 22.0 23.0 31.0 77.0 60.0
15 ⁰	14 ¹	16 ²	16 ²	1116 ⁶ 14.3 14.4 15.3 16.4 16.2 16.5 6.0
6.7	7.8	6.2	6.3	5.6 5.9 7.6 8.1 7.2 6.1 6.4 7.4
30	27	20	12	8 18 24 25 29 36 44
6 ¹	5 ⁰	26 ⁸	27 ⁸	1128 ⁰ 27 ⁹ 28 ³ 26 ³ 23 ¹
UP 6.3	5.4	5.8	4.8	4.6 5.2 4.3 5.7 9.5 level
30	19	13.5	12	11 16 20 24 43 26 ¹
UP 44 ⁸	40 ⁵	41 ⁰	40 ¹	1141 ¹ 40 ² 40 ² 45 ² 45.1 48 ⁵
3.4	6.2	10.5	10.0	10.9 10.2 9.9 9.9 10.1 10.8 5.2 5.9 2.5
34	21	15	10	7 5.5 3 12 15 23 30 40
		51 ⁰	45 ²	45.1
UP	0.0	5.8	5.9	
	9.5	7		
57 ⁵	58 ¹	54.4	52 ⁵	50.9 52 ¹ 1152 ³ 52 ⁰ 51 ⁵ 52 ³ 56.7
21	21	58	47	4.3 5.1 7.5 7.9 8.2 8.7 7.9 3.5 level
30	24	18 ²	15	13 11 10 13 14 17 22
63 ¹	63 ⁵	63 ⁷	60 ⁴	59.2 60 ⁴ 1160.8 60 ⁴ 61 ² 62 ⁵
UP 5.4	5.3	5.0	5.3	5.8 5.3 7.9 8.3 6.9 5.2 level yd drive
36	25	18	12	10 7.5 7.8 9 14 20 30
63 ³	64 ³	62 ⁵	62 ²	1162 ⁵ 63 ³ 62 ⁷ 61 ³ 64 ³ 64 ⁰
5.5	4.4	4.4	6.2	5.8 5.2 5.2 5.5 6.0 6.8 4.4 4.7 level lane
33	27	19 ⁰	14 ⁵	11 7 11 13 ² 19 30

STA.	B. S.	H. I.	F. S.	ELEVA.	GRADE	CUT OR	
						LEFT	G.
BM	6.34	1107.21		1100.87			
TP	0.24	1095.57	11.88	1095.33			
TP	0.35	1084.18	11.74	1093.53			
28-50			1.93				
29+00			6.6				
TP	0.33	1073.72	10.79	1073.39			
28+50			2.1				
TP			10.83	1062.89		TOP	27+50 ROW
BM SET 1952				1055.87			

FILL	AREA		CUBIC YARDS	
	RIGHT	EXCAVA	EXCAVA	EMBANK.

34498 S₁₀W 12° C₁ TELPA

S₁₀W N. SIDE MOST S ELY WILLOW ± 60' S OF CULVERT AT
STA 26+50

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

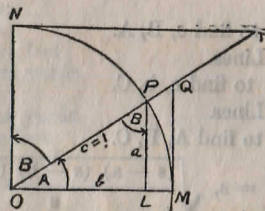


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Lines.

Given A, B, c; to find a, b, C.

Use Law of Lines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
$\frac{1}{16}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	$\frac{1}{16}$
$\frac{1}{8}$.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	$\frac{1}{8}$
$\frac{3}{16}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	$\frac{3}{16}$
$\frac{1}{4}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	$\frac{1}{4}$
$\frac{5}{16}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	$\frac{5}{16}$
$\frac{3}{8}$.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	$\frac{3}{8}$
$\frac{7}{16}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	$\frac{7}{16}$
$\frac{1}{2}$.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	$\frac{1}{2}$
$\frac{9}{16}$.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	$\frac{9}{16}$
$\frac{5}{8}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688	$\frac{5}{8}$
$\frac{11}{16}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	$\frac{11}{16}$
$\frac{3}{4}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	$\frac{3}{4}$
$\frac{13}{16}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	$\frac{13}{16}$
$\frac{7}{8}$.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	$\frac{7}{8}$
$\frac{15}{16}$.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	$\frac{15}{16}$
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.0000	1
	0	1	2	3	4	5	6	7	8	9	10	11	

TABLE IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links
360°	= 21600'	= 1296000"
Radius	= arc of 57.2957790°	
Arc of 1°	(radius = 1)	= .017453292
Arc of 1'	(radius = 1)	= .000290888
Arc of 1"	(radius = 1)	= .000004848

$$\pi = 3.141592654 \quad \sqrt{\frac{1}{4}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163 \quad \sqrt[3]{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776 \quad \pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167 \quad \frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776 \quad \sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205 \quad \frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in 11½ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{Mv^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE.

Horizontal Distance = R - R sin² a + C cos a

Vertical Distance = R ½ sin 2 a + C sin a

R = Reading × $\frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

TABLE VI (continued)
SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	deg
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	1.041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3097	969	.3190	37
53	986	.3270	8004	.3351	8021	.3452	8039	.3514	8056	.4106	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4064	175	.4193	35
55	192	.4281	208	.4370	225	.4460	241	.4550	258	.4604	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5198	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.5792	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31
59	572	.6643	587	.6753	601	.6864	616	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	1.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10
80	848	5.6713	9353	5.7694	9358	5.8708	9363	5.9758	9368	6.0844	9372	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	995	31.242	996	34.368	997	38.189	997	42.964	998	49.104	1
89	999	57.290	999	68.750	999	85.940	999	114.58	1.000	171.88	1.000	343.77	0
90	60'	60'	50'	50'	40'	40'	30'	30'	20'	30'	10'	10'	deg
	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	deg

TABLE VII
RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16-6	21	346-6	41	676-6	61	1006-6	81	1336-6
2	33-0	22	363-0	42	693-0	62	1023-0	82	1353-0
3	49-6	23	379-6	43	709-6	63	1039-6	83	1369-6
4	66-0	24	396-0	44	726-0	64	1056-0	84	1386-0
5	82-6	25	412-6	45	742-6	65	1072-6	85	1402-6
6	99-0	26	429-0	46	759-0	66	1089-0	86	1419-0
7	115-6	27	445-6	47	775-6	67	1105-6	87	1435-6
8	132-0	28	462-0	48	792-0	68	1122-0	88	1452-0
9	148-6	29	478-6	49	808-6	69	1138-6	89	1468-6
10	165-0	30	495-0	50	825-0	70	1155-0	90	1485-0
11	181-6	31	511-6	51	841-6	71	1171-6	91	1501-6
12	198-0	32	528-0	52	858-0	72	1188-0	92	1518-0
13	214-6	33	544-6	53	874-6	73	1204-6	93	1534-6
14	231-0	34	561-0	54	891-0	74	1221-0	94	1551-0
15	247-6	35	577-6	55	907-6	75	1237-6	95	1567-6
16	264-0	36	594-0	56	924-0	76	1254-0	96	1584-0
17	280-6	37	610-6	57	940-6	77	1270-6	97	1600-6
18	297-0	38	627-0	58	957-0	78	1287-0	98	1617-0
19	313-6	39	643-6	59	973-6	79	1303-6	99	1633-6
20	330-0	40	660-0	60	990-0	80	1320-0	100	1650-0

TABLE VIII
LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0-7.92	18	11-10.56	35	23-1.20	52	34-3.84	69	45-6.48	86	56-9.12
2	1-3.84	19	12-6.48	36	23-9.12	53	34-11.76	70	46-2.40	87	57-5.04
3	1-11.76	20	13-2.40	37	24-5.04	54	35-7.68	71	46-10.32	88	58-0.96
4	2-7.68	21	13-10.32	38	25-0.96	55	36-3.60	72	47-6.24	89	58-8.88
5	3-3.60	22	14-6.24	39	25-8.88	56	36-11.52	73	48-2.16	90	59-4.80
6	3-11.52	23	15-2.16	40	26-4.80	57	37-7.44	74	48-10.08	91	60-0.72
7	4-7.44	24	15-10.08	41	27-0.72	58	38-3.36	75	49-6.00	92	60-8.64
8	5-3.36	25	16-6.00	42	27-8.64	59	38-11.28	76	50-1.92	93	61-4.56
9	5-11.28	26	17-1.92	43	28-4.56	60	39-7.20	77	50-9.84	94	62-0.48
10	6-7.20	27	17-9.84	44	29-0.48	61	40-3.12	78	51-5.76	95	62-8.40
11	7-3.12	28	18-5.76	45	29-8.40	62	40-11.04	79	52-1.68	96	63-4.32
12	7-11.04	29	19-1.68	46	30-4.32	63	41-6.96	80	52-9.60	97	64-0.24
13	8-6.96	30	19-9.60	47	31-0.24	64	42-2.88	81	53-5.52	98	64-8.16
14	9-2.88	31	20-5.52	48	31-8.16	65	42-10.80	82	54-1.44	99	65-4.08
15	9-10.80	32	21-1.44	49	32-4.08	66	43-6.72	83	54-9.36	100	66-0.00
16	10-6.72	33	21-9.36	50	33-0.00	67	44-2.64	84	55-5.28	101	66-7.92
17	11-2.64	34	22-5.28	51	33-7.92	68	44-10.56	85	56-1.20	102	67-3.84

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30°
1°	50.00	.218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10'	58.34	.297	5° C.	10'	560.11	27.313	5° C.	10'	1070.6	99.155	5° C.
20'	66.67	.388	T	20'	568.53	28.137	T	20'	1079.2	100.75	T
30'	75.01	.491	.03	30'	576.95	28.974	.03	30'	1087.8	102.35	.13
40'	83.34	.606	E	40'	585.36	29.824	E	40'	1096.4	103.97	.10
50'	91.68	.733	.001	50'	593.79	30.686	.001	50'	1105.1	105.60	.013
2°	100.01	.873	10° C.	12°	602.21	31.561	10° C.	22°	1113.7	107.24	10° C.
10'	108.35	1.024	T	10'	610.64	32.447	T	10'	1122.4	108.90	T
20'	116.68	1.188	.06	20'	619.07	33.347	.06	20'	1131.0	110.57	.13
30'	125.02	1.364	E	30'	627.50	34.259	E	30'	1139.7	112.25	E
40'	133.36	1.552	.003	40'	635.93	35.183	.003	40'	1148.4	113.95	.025
50'	141.70	1.752	15° C.	50'	644.37	36.120	15° C.	50'	1157.0	115.66	15° C.
3°	150.04	1.964	T	13°	652.81	37.070	T	23°	1165.7	117.38	T
10'	158.38	2.188	.06	10'	661.25	38.031	.06	10'	1174.4	119.12	.13
20'	166.72	2.425	E	20'	669.70	39.006	E	20'	1183.1	120.87	E
30'	175.06	2.674	.003	30'	678.15	39.993	.003	30'	1191.8	122.63	.19
40'	183.40	2.934	T	40'	686.60	40.992	T	40'	1200.5	124.41	T
50'	191.74	3.207	10° C.	50'	695.06	42.004	10° C.	50'	1209.2	126.20	10° C.
4°	200.08	3.492	T	14°	703.51	43.029	T	24°	1217.9	128.00	T
10'	208.43	3.790	.06	10'	711.97	44.066	.06	10'	1226.6	129.82	.13
20'	216.77	4.099	E	20'	720.44	45.116	E	20'	1235.3	131.65	E
30'	225.12	4.421	.003	30'	728.90	46.178	.003	30'	1244.0	133.50	.19
40'	233.47	4.755	T	40'	737.37	47.253	T	40'	1252.8	135.35	T
50'	241.81	5.100	15° C.	50'	745.85	48.341	15° C.	50'	1261.5	137.23	15° C.
5°	250.16	5.459	T	15°	754.32	49.441	T	25°	1270.2	139.11	T
10'	258.51	5.829	.09	10'	762.80	50.554	.09	10'	1279.0	141.01	.29
20'	266.86	6.211	E	20'	771.29	51.679	E	20'	1287.7	142.93	E
30'	275.21	6.606	.004	30'	779.77	52.818	.004	30'	1296.5	144.85	.13
40'	283.57	7.013	T	40'	788.26	53.969	T	40'	1305.3	146.79	T
50'	291.92	7.432	10° C.	50'	796.75	55.132	10° C.	50'	1314.0	148.75	10° C.
6°	300.28	7.863	T	16°	805.25	56.309	T	26°	1322.8	150.71	T
10'	308.64	8.307	.06	10'	813.75	57.498	.06	10'	1331.6	152.69	.13
20'	316.99	8.762	E	20'	822.25	58.699	E	20'	1340.4	154.69	E
30'	325.35	9.230	.003	30'	830.76	59.914	.003	30'	1349.2	156.70	.19
40'	333.71	9.710	T	40'	839.27	61.141	T	40'	1358.0	158.72	T
50'	342.08	10.202	15° C.	50'	847.78	62.381	15° C.	50'	1366.8	160.76	15° C.
7°	350.44	10.707	T	17°	856.30	63.634	T	27°	1375.6	162.81	T
10'	358.81	11.224	.06	10'	864.82	64.900	.06	10'	1384.4	164.86	.13
20'	367.17	11.753	E	20'	873.35	66.178	E	20'	1393.2	166.95	E
30'	375.54	12.294	.003	30'	881.88	67.470	.003	30'	1402.0	169.04	.19
40'	383.91	12.847	T	40'	890.41	68.774	T	40'	1410.9	171.15	T
50'	392.28	13.413	10° C.	50'	898.95	70.091	10° C.	50'	1419.7	173.27	10° C.
8°	400.66	13.991	T	18°	907.49	71.421	T	28°	1428.6	175.41	T
10'	409.03	14.582	.06	10'	916.03	72.764	.06	10'	1437.4	177.55	.13
20'	417.41	15.184	E	20'	924.58	74.119	E	20'	1446.3	179.72	E
30'	425.79	15.799	.003	30'	933.13	75.488	.003	30'	1455.1	181.89	.19
40'	434.17	16.426	T	40'	941.69	76.869	T	40'	1464.0	184.08	T
50'	442.55	17.065	15° C.	50'	950.25	78.264	15° C.	50'	1472.9	186.29	15° C.
9°	450.93	17.717	T	19°	958.81	79.671	T	29°	1481.8	188.51	T
10'	459.32	18.381	.06	10'	967.38	81.092	.06	10'	1490.7	190.74	.13
20'	467.71	19.058	E	20'	975.96	82.525	E	20'	1499.6	192.99	E
30'	476.10	19.746	.003	30'	984.53	83.972	.003	30'	1508.5	195.25	.19
40'	484.49	20.447	T	40'	993.12	85.431	T	40'	1517.4	197.53	T
50'	492.88	21.161	10° C.	50'	1001.7	86.904	10° C.	50'	1526.3	199.82	10° C.
10°	501.28	21.887	T	20°	1010.3	88.389	T	30°	1535.3	202.12	T
10'	509.68	22.624	.06	10'	1018.9	89.888	.06	10'	1544.2	204.44	.13
20'	518.08	23.375	E	20'	1027.5	91.399	E	20'	1553.1	206.77	E
30'	526.48	24.138	.003	30'	1036.1	92.924	.003	30'	1562.0	209.12	.19
40'	534.89	24.913	T	40'	1044.7	94.462	T	40'	1571.0	211.48	T
50'	543.29	25.700	15° C.	50'	1053.3	96.013	15° C.	50'	1580.0	213.86	15° C.

T = R tan 1/2 I

E = R exsec 1/2 I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	387.4	+	51°	2732.9	618.4	+
10'	1598.0	218.7	5° C.	10'	2151.7	390.7	5° C.	10'	2743.1	622.8	5° C.
20'	1606.9	221.1	T	20'	2161.2	394.1	T	20'	2753.4	627.2	T
30'	1615.9	223.5	.13	30'	2170.8	397.4	.13	30'	2763.7	631.7	.21
40'	1624.9	226.0	E	40'	2180.3	400.8	E	40'	2773.9	636.2	E
50'	1633.9	228.4	.023	50'	2189.9	404.2	.023	50'	2784.2	640.7	.056
32°	1643.0	230.9	10° C.	42°	2199.4	407.6	10° C.	52°	2794.5	645.2	10° C.
10'	1652.0	233.4	T	10'	2209.0	411.1	T	10'	2804.9	649.7	T
20'	1661.0	235.9	.06	20'	2218.6	414.5	.06	20'	2815.2	654.3	.06
30'	1670.0	238.4	E	30'	2228.1	418.0	E	30'	2825.6	658.8	E
40'	1679.1	241.0	.013	40'	2237.7	421.4	.013	40'	2835.9	663.4	.056
50'	1688.1	243.5	15° C.	50'	2247.3	425.0	15° C.	50'	2846.3	668.0	15° C.
33°	1697.2	246.1	T	43°	2257.0	428.5	T	53°	2856.7	672.7	T
10'	1706.3	248.7	.26	10'	2266.6	432.0	.26	10'	2867.1	677.3	.26
20'	1715.3	251.3	E	20'	2276.2	435.6	E	20'	2877.5	682.0	E
30'	1724.4	253.9	.046	30'	2285.9	439.2	.046	30'	2888.0	686.7	.046
40'	1733.5	256.5	T	40'	2295.6	442.8	T	40'	2898.4	691.4	T
50'	1742.6	259.1	10° C.	50'	2305.2	446.4	10° C.	50'	2908.9	696.1	10° C.
34°	1751.7	261.8	T	44°	2314.9	450.0	T	54°	2919.4	700.9	T
10'	1760.8	264.5	.40	10'	2324.6	453.6	.40	10'	2929.9	705.7	.40
20'	1770.0	267.2	E	20'	2334.3	457.3	E	20'	2940.4	710.5	E
30'	1779.1	269.9	.070	30'	2344.1	461.0	.070	30'	2951.0	715.3	.070
40'	1788.2	272.6	T	40'	2353.8	464.6	T	40'	2961.5	720.1	T
50'	1797.4	275.3	15° C.	50'	2363.5	468.4	15° C.	50'	2972.1	725.0	15° C.
35°	1806.6	278.1	T	45°	2373.3	472.1	T	55°	2982.7	729.9	T
10'	1815.7	280.8	.50	10'	2383.1	475.8	.50	10'	2993.3	734.8	.50
20'	1824.9	283.6	E	20'	2392.8	479.6	E	20'	3003.9	739.7	E
30'	1834.1	286.4	.070	30'	2402.6	483.4	.070	30'	3014.5	744.6	.070
40'	1843.3	289.2	T	40'	2412.4	487.2	T	40'	3025.2	749.6	T
50'	1852.5	292.0	10° C.	50'	2422.3	491.0	10° C.	50'	3035.8	754.6	10° C.
36°	1861.7	294.9	T	46°	2432.1	494.8	T	56°	3046.5	759.6	T
10'	1870.9	297.7	.53	10'	2441.9	498.7	.53	10'	3057.2	764.6	.53
20'	1880.1	300.6	E	20'	2451.8	502.5	E	20'	3067.9	769.7	E
30'	1889.4	303.5	.070	30'	2461.7	506.4	.070	30'	3078.7	774.7	.070
40'	1898.6	306.4	T	40'	2471.5	510.3	T	40'	3089.4	779.8	T
50'	1907.9	309.3	15° C.	50'	2481.4	514.3	15° C.	50'	3100.2	784.9	15° C.
37°	1917.1	312.2	T	47°	2491.3	518.2	T	57°	3110.9	790.1	T
10'	1926.4	315.2	.093	10'	2501.2	522.2	.093	10'	3121.7	795.2	.093
20'	1935.7	318.1	E	20'	2511.2	526.1	E	20'	3132.6	800.4	E
30'	1945.0	321.1	.117	30'	2521.1	530.1	.117	30'	3143.4	805.6	.117
40'	1954.3	324.1	T	40'	2531.1	534.2	T	40'	3154.2	810.9	T
50'	1963.6	327.1	10° C.	50'	2541.0	538.2	10° C.	50'	3165.1	816.1	10° C.
38°	1972.9	330.2	T	48°	2551.0	542.2	T	58°	3176.0	821.4	T
10'	1982.2	333.2	.117	10'	2561.0	546.3	.117	10'	3186.9	826.7	.117
20'	1991.5	336.3	E	20'	2571.0	550.4	E	20'	3197.8	832.0	E
30'	2000.9	339.3	.070								

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

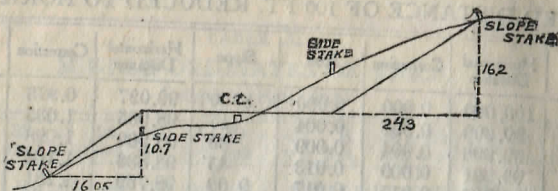
TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise	Slope	Horizontal Distance	Correction	Rise
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

For each foot take one one-hundredth of each reading.

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 10"	.50833	40' 30"	.67500	50' 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	40	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

1035.51

12.77

1023.04

1.69

1024.73

12.77

1011.96

2.27

1014.23

1032.40

117 233
55 W
51 79

7636.2
55 W

2092.2

3999.72

2241

1758.72

2845

5543.80

40

1543.80

5543.80

660

4883.80

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250-X



JJUU
660
488 W

cho

